BLAKEBOROUGH® TURBINE BYPASS VALVES









QUALITY ASSURANCE

Trillium is qualified to industry standards and working practices including:

- ASME BPVC Section III (N and NPT Stamp)
- NQA-1 Quality system
- 10CFR50 App. B
- 10CFR50 Part 21
- RCC-E
- RCC-M
- CSA Z299
- Performance testing and qualification to:

ASME QME-1

ASME B16.41

IEEE 323

IEEE 344

IEEE 382

- ISO 9001:2008
- ISO 14001
- PED 97/23/CE
- API Q1 TO API LICENCES:

API 6D (6D-0182)

API 6A (64-0445)

- OHSAS 18001
- ATEX 94/9/CE
- Lean manufacturing practices

















ATWOOD & MORRILL®

Engineered Isolation & Check Valves

BATLEY VALVE®

Butterfly Valves

RED POINT®

Tailor-Made Valve

BLAKEBOROUGH®

Control, Choke & Steam Condtioning Valves

HOPKINSONS®

Isolation Valves

SARASIN-RSBD®

Safety & Safety Relief Valves

SEBIM®

Nuclear Pilot Operated Safety Valves

TRICENTRIC®

Triple Offset Butterfly Valves

Portfolio of engineered service solutions and aftermarket support

A PROVEN TRACK RECORD

We have extensive references and a proven track record in the supply of valves across a number of key industries. Our valves are industry renowned brands, each with an established reputation for quality engineering and reliability.

VALVE TESTING

All pressure containing items are hydrostatically tested, seat leakage tested and functionally tested. We can also perform gas, packing emission, cryogenic and advanced functional testing, as well as seismic testing for nuclear applications.

MATERIAL TESTING

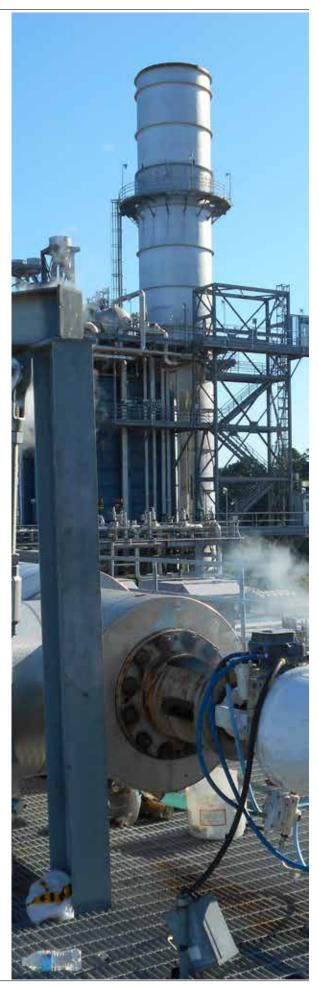
- Non-destructive examination by radiography, ultrasonics, magnetic particle and liquid penetrant
- Chemical analysis by computer controlled direct reading emission spectrometer
- Mechanical testing for tensile properties at ambient and elevated temperatures, bend and hardness testing. Charpy testing at ambient, elevated and sub-zero temperatures

AFTERMARKET SOLUTIONS

Our valve aftermarket solutions are based on our engineering heritage, applying our OEM knowledge and expertise to maintenance strategies, life extension and upgrade projects. Trillium Control & Choke Valves provides a wide range of control valves for the process industry. These include severe service, choke, desuperheating and turbine bypass applications. Our world-wide reputation is based on engineering excellence applied to a comprehensive range of specialist products and effective customer support.

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The Trillium BV995 Turbine Bypass Valve is a highly sophisticated engineered control device. Conceptually, it is required to accurately control multiple operational variables, provide system protection to both upstream and downstream plant components, and sometimes perform these tasks all in a fraction of a second. Depending on the overall system size, bypass mode of operation and customer preference, there is almost an endless selection of options and configurations that can be applied to the BV995 bypass valve construction. The Trillium BV995 Turbine Bypass Valve design can be varied to accommodate the particular plant design, size, and application. It is available in a range of options and configurations to assure optimum performance regardless of the mode of operation.

HIGH PRESSURE (HP) BYPASS VALVE

The high pressure (HP) bypass valves are subject to some of the highest pressures and temperatures. They may be utilized in either a Parallel or Cascading Bypass System. If the plant is configured in a Parallel arrangement, the HP Bypass Valve will direct the outlet steam flow to the condenser. If the plant is configured as a Cascading system (the most common in today's plants) the steam will be directed to the Cold Reheat section of the boiler or steam generator. Regardless, these valves will warrant the highest pressure ratings which may go as high as ASME 4500. The valves are commonly manufactured from forged materials which allow for higher strength and ductility when compared to the equivalent cast material. The additional strength of the forged materials also provide greater manufacturing flexibility which allows for optimised contours and shapes that can result in thinner wall sections being applied to the valve body design. This helps in reducing the effect of thermal gradient stress across the body caused by the rapid and sudden opening of the valve during a turbine trip sequence

HRH BYPASS VALVE (MP, IP, OR HRH)

The Hot Reheat (HRH) bypass valves (sometimes referred to as Intermediate or Medium Pressure) are used to bypass steam to the condenser regardless of whether the bypass system is configured as parallel or cascading. The required flow coefficient, Cv, for these valves is often the largest in the system due to the combination of lower steam pressures and higher temperatures emanating from the re-heater. They are used to convert the HRH steam to conditions more acceptable for admission into the condenser. As a result of the high steam temperatures entering these valves, they normally require a significant amount of desuperheating flow to reduce the outlet enthalpy to acceptable condenser inlet conditions.



HRH Bypass valve

LOW PRESSURE BYPASS VALVE (LP)

The low pressure bypass valve is used to bypass the LP section of the turbine and also directs its steam discharge to the condenser. The low pressure valves are not subject to extremes of heat and pressure in the same way as the HP and HRH bypass valves. They are therefore mostly made from lower grade cast materials such as ASTM/ASME SA216 WCB or carbon steel forgings such as ASTMASME SA A105. Due to the lower inlet pressures and temperatures, the LP bypass design criteria are not as difficult and there are many possible valve solutions and configurations for this application.

BONNET DESIGN OPTIONS

In the design of any pressure vessel, there will always be a requirement to allow access to the inside of the component via the penetration of the pressure retaining boundary. In the case of a turbine bypass valve, this is usually facilitated by the valves bonnet. Under pressurized or operational conditions, the bonnet serves the same purpose as the vessel wall in securely containing the pressure and flow. However, when it is time for inspection or maintenance, the bonnet can be removed and access to the valve trim and seat can be afforded. Depending on the system pressures, valve size, and customer preference there are two main bonnet designs that are quite typical for turbine bypass valves.

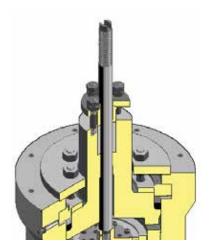
These are:

- · Bolted Mechanical Bonnet
- Pressure Seal or Pressure Assisted Bonnet



LP Bypass valve



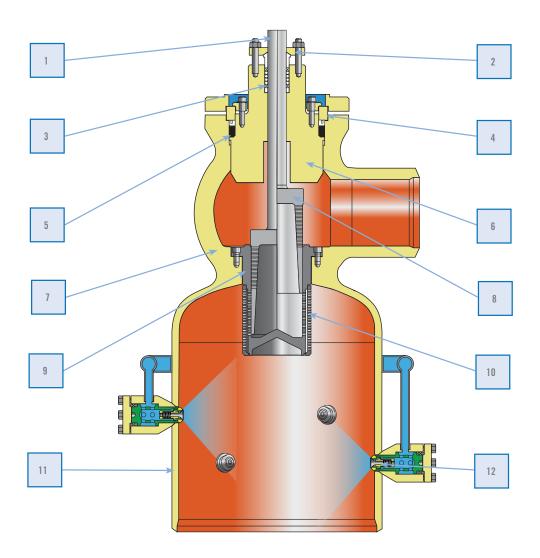


Pressure seal bonnet design



Typical bolted bonnet

STANDARD MATERIALS OF CONSTRUCTION



| PART NO. | DESCRIPTION | MATERIAL STANDARD | COMMENTS |
|----------|---------------------------|-----------------------------|------------------|
| 1 | Valve Stem | AISI 616 | Surface Hardened |
| 2 | Packing Hardware | AISI 420 | |
| 3 | Packing | Graphite | |
| 4 | Segment/Spacer Ring | SA182-F22/F91/F92 | |
| 5 | Pressure Seal Gasket | Graphite | SST Reinforced |
| 6 | Bonnet | SA105/SA182-F11,F22,F91/F92 | |
| 7 | Valve Body | SA105/SA182-F11,F22,F91/F92 | |
| 8 | Control Plug | SA182-F22/F91/F92 | Alloy 6 Overlay |
| 9 | Seat Ring | SA182-F22/F91/F92 | Alloy 6 Overlay |
| 10 | Pressure Reduction Stages | SA182-F22/F91/F92 | |
| 11 | Outlet | SA106/SA335-P11,P22,P91 | |
| 12 | VG Nozzle | AISI 410 | |

STANDARD MATERIALS OF CONSTRUCTION

Pressure Boundary Integrity

Bonnet closure provided in either a pressure seal (High Pressure) or bolted (Low Pressure) design

Low Stress Configuration

The inside and outside body contours are fully machined to assure smooth transition with little or no stress due to thermal or mechanical loading

Fully Serviceable Trim

Seat ring and pressure reduction stages are fully removable for service or modification

Customised Desuperheating

The size, number, and location of the spray nozzles is optimised for each application so as to achieve the most advantageous distribution and coverage of the flow stream

Leakage Minimised

Available with three different plug configurations including pressure balanced for Class IV and Pilot balanced for Class V

Inlet/Outlet Connections

Size and materials selected to match customer's requirements

Noise Attenuation

Pressure reduction accomplished via two coordinated control surfaces and 1 or 2 outlet diffusers. Pressure reduction ratios balanced to eliminiate unwanted noise and vibration

Water Injection

All desuperheating is conducted after the pressure reduction is complete, assuring little or no thermal shocking to termperature sensitive trim

Variable Geometry Nozzles

Spring-loaded, backpressure activated, variable geometry nozzles provide an excellent spray pattern for quick mixing and evaporation

Plug Configurations

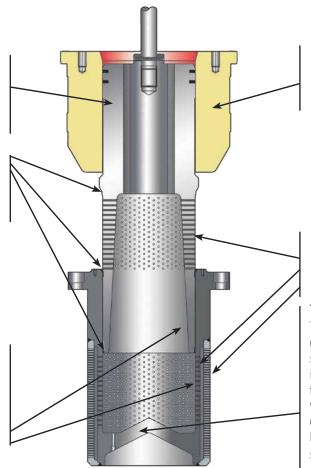
The control plug is available in either a balanced, unbalanced, or pilot balanced balanced, unbalanced, or pilot balanced actuating requirements

Hardened Surfaces

All seating and guide surfaces overlaid with alloy 6 material to provide smooth stroking and tight shut-off

Co-ordinated Control Surfaces

Trim provides a minimum of two stages of co-ordinated control and pressure reduction thus lowering noise and providing excellent rangeability



Hung Cage Trim

Allows for free axial expansion of the trim due to thermal expansion

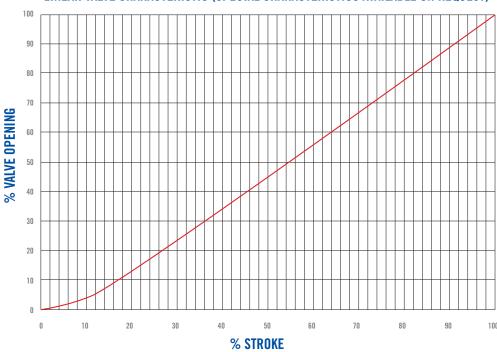
Low Noise Trim

Three stages of expansion controlled trim provide a solution to meet noise specifications

Trim Arrangement

The selection, number, and nesting of the appropriate pressure reduction stages is optimised to achieve a balance in the pressure drop ratio across the trim assembly and minimise noise and vibration. The plug has a single flow coefficient per valve size, the 2nd stage has five different capacities, and the 3rd stage has 10 different capacities. In this way, they can be mixed and matched to achieve maximum stability and control.

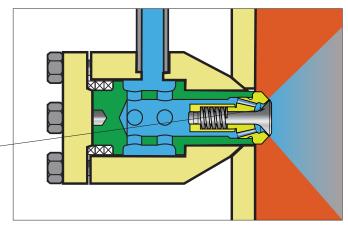
LINEAR VALVE CHARACTERISTIC (SPECIAL CHARACTERISTICS AVAILABLE ON REQUEST)



SPRAY NOZZLES

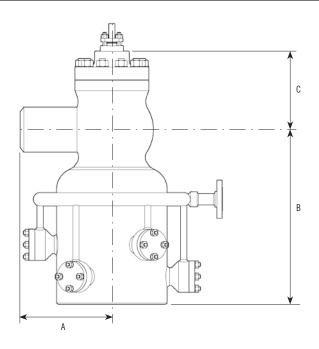
The advantage of the VG nozzle is its pressure activated variable geometry. No flow is allowed to pass through the nozzle until a definitive minimum pressure differential has been achieved. The established minimum pressure differential varies between each nozzle, but is normally in the 20-35 PSID (1.4-2.4 BarD) range. In this manner, the nozzle never has low flow spray pattern decay or collapse. If the differential should happen to fall below this minimum pressure limit, the flow element will re-seat itself and stop the flow of water until the pressure once again increases. As with most mechanical devices, there is an upper as well as a lower limit with respect to the allowable pressure differential. For long term performance, it is recommended that the nozzle not be used with differentials greaterthan 500 PSID or 35 BarD without consulting a Trillium X-Pert.





| VG FAMILY OF N | VG FAMILY OF NOZZLE SIZES | | | | | | | | | |
|----------------|---------------------------|-----|-----|-----|-----|----|-----|-----|-----|-----|
| Nozzle Size | 10 | 14 | 17 | 20 | 24 | 28 | 32 | 35 | 40 | 44 |
| Nozzle Cv | 0.5 | 1.2 | 1.4 | 1.9 | 2.5 | 3 | 3.4 | 3.6 | 4.4 | 4.8 |





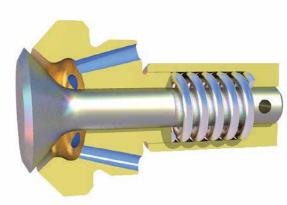
| BV995 BASIC DIMENSIONS | | | | | | | | | |
|------------------------|--------|------|------|------|------|-------------|--------------|--|--|
| MODEL | STROKE | CV | A | В | C | INLET RANGE | OUTLET RANGE | | |
| BV995-40 | 32 | 40 | 100 | 240 | 130 | 1"-4" | 6"-16" | | |
| BV995-50 | 40 | 60 | 130 | 300 | 160 | 1"-6" | 6"-16" | | |
| BV995-60 | 48 | 80 | 155 | 365 | 190 | 2"-6" | 8"-20" | | |
| BV995-70 | 56 | 110 | 180 | 425 | 220 | 2"-8" | 8"-20" | | |
| BV995-80 | 64 | 140 | 210 | 490 | 250 | 3"-8" | 8"-20" | | |
| BV995-90 | 72 | 175 | 230 | 550 | 280 | 3"-8" | 8"-20" | | |
| BV995-100 | 80 | 215 | 260 | 610 | 310 | 4"-10" | 10"-24" | | |
| BV995-110 | 88 | 260 | 290 | 670 | 350 | 4"-10" | 10"-24" | | |
| BV995-120 | 96 | 310 | 310 | 730 | 380 | 4"-10" | 12"-24" | | |
| BV995-130 | 104 | 360 | 340 | 790 | 410 | 4"-10" | 12"-24" | | |
| BV995-145 | 116 | 450 | 380 | 880 | 460 | 6"-12" | 14"-30" | | |
| BV995-160 | 128 | 550 | 420 | 980 | 500 | 6"-12" | 14"-30" | | |
| BV995-175 | 140 | 660 | 460 | 1070 | 550 | 6"-12" | 16"-30" | | |
| BV995-190 | 152 | 775 | 500 | 1160 | 600 | 8"-14" | 16"-30" | | |
| BV995-210 | 168 | 945 | 550 | 1280 | 660 | 8"-14" | 18"-32" | | |
| BV995-230 | 184 | 1135 | 600 | 1400 | 730 | 8"-14" | 18"-32" | | |
| BV995-250 | 200 | 1340 | 650 | 1520 | 790 | 10"-16" | 20"-36" | | |
| BV995-275 | 220 | 1620 | 720 | 1680 | 870 | 10"-16" | 20"-36" | | |
| BV995-300 | 240 | 1925 | 790 | 1830 | 950 | 10"-16" | 24"-48" | | |
| BV995-330 | 164 | 2325 | 860 | 2010 | 1040 | 12"-18" | 24"-48" | | |
| BV995-360 | 288 | 2765 | 940 | 2200 | 1140 | 14"-20" | 30"-60" | | |
| BV995-400 | 320 | 3410 | 1050 | 2440 | 1260 | 16"-22" | 30"-60" | | |
| BV995-435 | 348 | 4030 | 1140 | 2660 | 1370 | 18"-24" | 30"-60" | | |
| BV995-480 | 384 | 4860 | 1260 | 2930 | 1510 | 20"-26" | 36"-72" | | |
| BV995-525 | 420 | 5900 | 1380 | 3200 | 1660 | 22"-28" | 36"-72" | | |
| BV995-575 | 460 | 7000 | 1500 | 3510 | 1810 | 24"-30" | 42"-72" | | |
| BV995-630 | 504 | 8400 | 1650 | 3840 | 1990 | 30"-36" | 42"-72" | | |

DESUPERHEATING FUNCTION

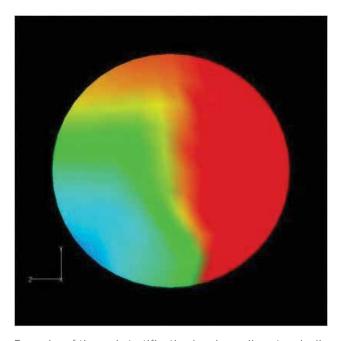
For turbine bypass applications, the most common nozzle used with the Trillium Bypass valves is the BV984-VG (Variable Geometry) nozzle. It is a back pressure activated, variable geometry injection device.

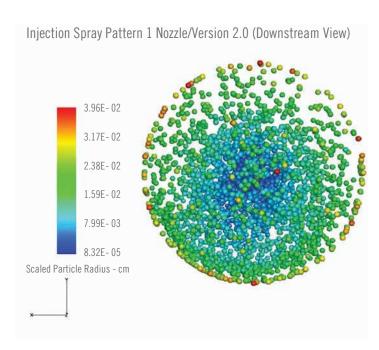
Depending on the required spray water requirements, a number of nozzles are located radially around the outlet pipe. Selecting the right number of nozzles with a suitable pressure drop across each nozzle is crucial to obtaining an efficient spray injection pattern in the valve outlet. The number and location of the nozzles is critical to assure good spray penetration, complete flow area coverage, and minimise the formation of thermal stratification, a problem particularly prone in large diameter pipelines.

In the case of the BV984-VG nozzle, the internal spring keeps the flow element seated until a minimum pressure differential is reached. At this point, increasing pressure surpasses the seating load of the spring and the flow element moves in an axial direction. This axial motion of the flow element with respect to the spray head creates an annular flow area between the two components. The flow through the annular area extrudes a thin sheet of water with a uniform thickness. Due to pressure perturbations, the sheet almost immediately begins to breakup, first into ligaments and then further into fine spray particles in the range of 50- $200\mu m$.



BV984-VG Nozzle Design





Examples of thermal stratification in a large diameter pipeline and analysis of spray particle distribution and coverage in a bypass application.

BACKPRESSURE DEVICE

The backpressure device, also referred to as a dump tube or sparger, is utilised to create a positive pressure downstream of the valve. Without this device, the vacuum conditions of the condenser would exist in the discharge piping.

At these extremely low pressures, the velocity of the steam exiting the valve would reach sonic or choked conditions almost immediately unless the outlet pipe size and resultant cross-sectional flow area, were sized to accommodate the large specific volume of the free expanding steam. As this is normally not economically feasible or logistically possible, the backpressure device is installed to provide a fixed resistance to the flow entering the condenser.

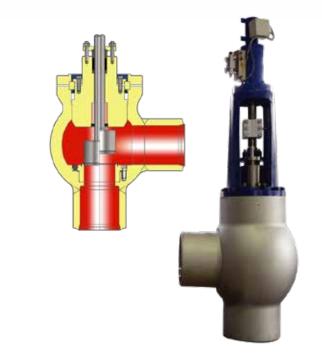
Trillium can provide engineering assistance or complete production of the backpressure device for whatever the application requires.



The BV995 Turbine Bypass Valve is capable of providing excellent shutoff; and therefore no additional shut-off or isolation valves are required. However, if code or mode of operation should deem the use of an independent stop valve for either redundancy or shut-off safety function, Trillium offers the BV995SV. The design includes many of the physical features of the bypass valve including forged contoured bodies, matching inlet & outlet sizes, field removable seat ring, various body materials, and bonnet designs.

The BV995SV is designed to withstand the thermal cycling requirements of bypass service while at the same time providing low pressure drop and a high degree of seat integrity even when vacuum conditions are involved. It is recommended that the stop valves should remain open when the plant is in operation to assist in the preheating of the bypass valve.











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